

CHAPTER 6 - FIR Filters

6.1

Passband edge at 1.25 kHz

For 40 dB rejection need Hanning window transition bandwidth = $\frac{3.1}{N\Delta t}$

where $\Delta t = 10^{-4}$ and $N = 21$

Therefore transition bandwidth = $\frac{3.1}{21} \times 10^4 = 1.48 \times 10^3 = 1.48$ kHz

Stopband starts at $1.25 + 1.48 = 2.73$ kHz and goes up to 5 kHz (folding frequency), OR possibly $10 - 2.73 = 7.27$ kHz.

6.2

$$1.25 \text{ kHz} = \frac{f_s}{8}$$

Now using $\omega = 2\pi f$ and $d\omega = 2\pi df$:-

$$c_n = \frac{2}{f_s} \int_0^{\frac{f_s}{2}} H_D(f) \cos \frac{2\pi n f}{f_s} df$$

$$= \frac{2}{f_s} \int_0^{\frac{f_s}{2}} 4 \cos \frac{2\pi n f}{f_s} df$$

$$= \left[4 \frac{2}{f_s} \frac{f_s}{2\pi n} \sin \frac{2\pi n f}{f_s} \right]_0^{\frac{f_s}{2}}$$

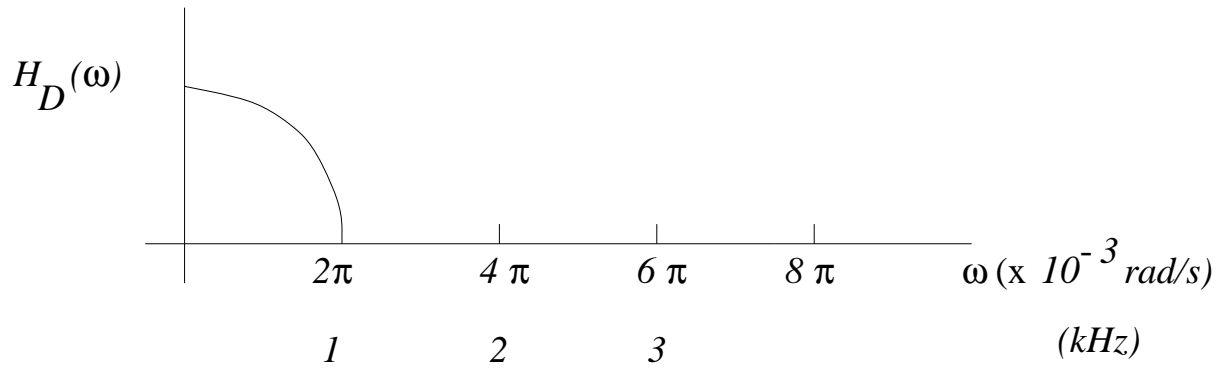
$$= \frac{4 \sin \frac{2\pi n f_s}{8f_s}}{\pi n} = \frac{\sin \frac{\pi n}{4}}{\frac{\pi n}{4}}$$

c_0	$= 1$	$= a_{10}$	
c_1	$= 0.9$	$= a_9$	$= a_{11}$
c_2	$= 0.64$	$= a_8$	$= a_{12}$
c_3	$= 0.3$	$= a_7$	$= a_{13}$
c_4	$= 0$	$= a_6$	$= a_{14}$
c_5	$= -0.18$	$= a_5$	$= a_{15}$
c_6	$= -0.212$	$= a_4$	$= a_{16}$
c_7	$= -0.128$	$= a_3$	$= a_{17}$
c_8	$= 0$	$= a_2$	$= a_{18}$

$$\begin{aligned} c_9 &= 0.1 & = a_1 & = a_{19} \\ c_{10} &= 0.128 & = a_0 & = a_{20} \end{aligned}$$

These values would not be used in practice without including a window function!

6.3.



Time between samples

$$\Delta t = \frac{1}{8 \times 10^3} \text{ s}$$

$$\text{Sampling frequency } \omega_s = 2\pi (8 \times 10^3) \text{ rad/s}$$

$$H_D(\omega) = \begin{cases} \cos(2\omega\Delta t), & \omega < \frac{\pi}{4\Delta t} \\ 0, & \text{elsewhere} \end{cases}$$

Impulse response calculation

$$\begin{aligned} c_n &= \frac{\Delta t}{\pi} \int_0^{\frac{\pi}{4\Delta t}} H_D(\omega) \cos(n\omega\Delta t) d\omega \\ &= \frac{\Delta t}{\pi} \int_0^{\frac{\pi}{4\Delta t}} \cos(2\omega\Delta t) \cos(n\omega\Delta t) d\omega \\ &= \frac{\Delta t}{2\pi} \int_0^{\frac{\pi}{4\Delta t}} \{ \cos((2+n)\omega\Delta t) + \cos((2-n)\omega\Delta t) \} d\omega \end{aligned}$$

$$\begin{aligned}
 &= \frac{\Delta t}{2\pi} \left[\frac{\sin((2+n)\omega\Delta t)}{(2+n)\Delta t} + \frac{\sin((2-n)\omega\Delta t)}{(2-n)\Delta t} \right]_0^{\frac{\pi}{4\Delta t}} \\
 &= \frac{1}{2\pi} \left[\frac{\sin\left((2+n)\frac{\pi}{4}\right)}{(2+n)} + \frac{\sin\left((2-n)\frac{\pi}{4}\right)}{(2-n)} \right] \\
 &= \frac{1}{8} \left[\text{sinc}\left((2+n)\frac{\pi}{4}\right) + \text{sinc}\left((2-n)\frac{\pi}{4}\right) \right]
 \end{aligned}$$

Therefore $c_0 = 0.16$
 $c_1 = 0.15$
 $c_2 = 0.125$ (sinc 0 = 1 !)
 $c_3 = 0.09$ etc

Apply Hanning window

Filter has $2M + 1 = 15$ taps

$\Rightarrow M = 7$

$$w_n = \frac{1}{2} \left\{ 1 + \cos\left(\frac{n\pi}{7}\right) \right\}$$

$$c'_n = w_n c_n$$

Therefore $c'_0 = 1 \times 0.16 = 0.16$

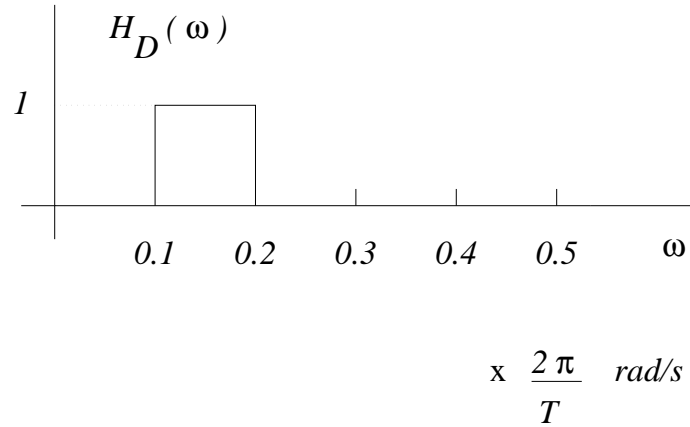
$c'_1 = 0.95 \times 0.15 = 0.14$

$c'_2 = 0.81 \times 0.125 = 0.10$

$c'_3 = 0.61 \times 0.09 = 0.05$

etc.

6.4.



$$\begin{aligned}
 c_n &= \frac{\Delta t}{\pi} \int_{\frac{\pi}{5\Delta t}}^{\frac{2\pi}{5\Delta t}} \cos(n\omega\Delta t) d\omega \\
 &= \frac{\Delta t}{\pi} \left[\frac{\sin(n\omega\Delta t)}{n\Delta t} \right]_{\frac{\pi}{5\Delta t}}^{\frac{2\pi}{5\Delta t}} \\
 &= \frac{1}{\pi} \left\{ \frac{\sin\left(\frac{2\pi n}{5}\right)}{n} - \frac{\sin\left(\frac{\pi n}{5}\right)}{n} \right\}
 \end{aligned}$$

Apply Hanning window

The filter has $(2M + 1) = 17$ taps

$$\Rightarrow M = 8$$

$$w_n = \frac{1}{2} \left\{ 1 + \cos \frac{(n\pi)}{8} \right\}$$

$$c'_n = w_n c_n$$

$$c'_0 = 1.0 \times 0.2 = 0.2$$

$$c'_1 = 0.96 \times 0.116 = 0.112$$

$$c'_2 = 0.85 \times -0.058 = -0.05$$

etc.

6.5.

For a low-pass filter ($0 - f_s/5$)

$$\begin{aligned}
 c_n &= \frac{\Delta t}{2\pi} \int_0^{2\pi/\Delta t} H_D(\omega) \cos \frac{2\pi n\omega}{\omega_s} d\omega \\
 &= \frac{\Delta t}{\pi} \int_0^{\omega_s/5} \sqrt{10} \cos \frac{2\pi n\omega}{\omega_s} d\omega \\
 &= \left[\frac{\Delta t}{\pi} \sqrt{10} \frac{\omega_s}{2\pi n} \sin \frac{2\pi n\omega}{\omega_s} \right]_0^{\omega_s/5} \\
 &= \sqrt{10} \frac{\sin \frac{2\pi n\omega_s}{5 \omega_s}}{\pi n} = \frac{2\sqrt{10}}{5} \frac{\sin \frac{2\pi n}{5}}{\frac{2\pi n}{5}} \\
 &= 1.265 \frac{\sin \frac{2\pi n}{5}}{\frac{2\pi n}{5}} \text{ or } \left(1.006 \frac{\sin \frac{2\pi n}{5}}{n} \right)
 \end{aligned}$$

For unweighted filters substitution for n yields:

$$\begin{array}{rcccccccc}
 n & = & 0, & 1, & 2, & 3, & 4, & 5, & 6 \\
 c_{n1} & = & 1.265, & 0.95, & 0.30, & -0.20, & -0.24, & 0, & 0.16
 \end{array}$$

For narrowband low-pass filter ($0 - f_s/10$)

$$\begin{aligned}
 c_n &= \left[\frac{\Delta t}{2\pi} \sqrt{10} \frac{\omega_s}{2\pi n} \sin \frac{2\pi n\omega}{\omega_s} \right]_0^{\omega_s/10} \\
 &= \sqrt{10} \sin \frac{2\pi n\omega_s}{10 \omega_s} = \frac{\sqrt{10}}{5} \frac{\sin \frac{2\pi n}{10}}{\frac{2\pi n}{10}}
 \end{aligned}$$

and again substitution for an unweighted filter gives:

$$\begin{array}{rcccccccc}
 n & = & 0, & 1, & 2, & 3, & 4, & 5, & 6 \\
 c_{n2} & = & 0.632, & 0.59, & 0.48, & 0.32, & 0.15, & 0, & -0.103
 \end{array}$$

The number of taps required for $H_2(\omega)$ is determined by the transition bandwidth of this filter. If the transition band is the same as for $H_1(\omega)$, 31 taps would suffice for $H_2(\omega)$ as well. Alternatively, if the transition bandwidth for $H_2(\omega)$ was one half of that for $H_1(\omega)$, the $H_2(\omega)$ filter will need twice the number of coefficients, i.e. it would be a 63 tap design.

Combining these filters gives:

n	=	0,	1,	2,	3,	4,	5,	6, etc
c_{n1}	=	1.265,	0.95,	0.296,	-0.197,	-0.239,	0,	0.16
$-c_{n2}$	=	0.632,	0.59,	0.48,	0.32,	0.15,	0,	-0.10
$c_{n1} - c_{n2}$	=	0.632,	0.36	-0.18,	-0.517,	-0.389,	0,	0.26

Now these weights now have to be converted into a symmetrical filter, where $n = 0$ gives the centre tap weight value.